

3D Geomechanical Modelling of CO₂ Storage with Focus on Fault Stability

Emil Gallyamov^{1,2}, B. Lecampion¹, N. Richart²,
G. Anciaux², J.F. Molinari²

¹Geo-Energy Laboratory

²Computational Solid Mechanics Laboratory

École Polytechnique Fédérale de Lausanne (EPFL),
Switzerland

MEGA Seminar

21st March 2024



Prof. Brice Lecampion
Geo-Energy Lab,
Gaznat Chair on Geo-
energy,
EPFL



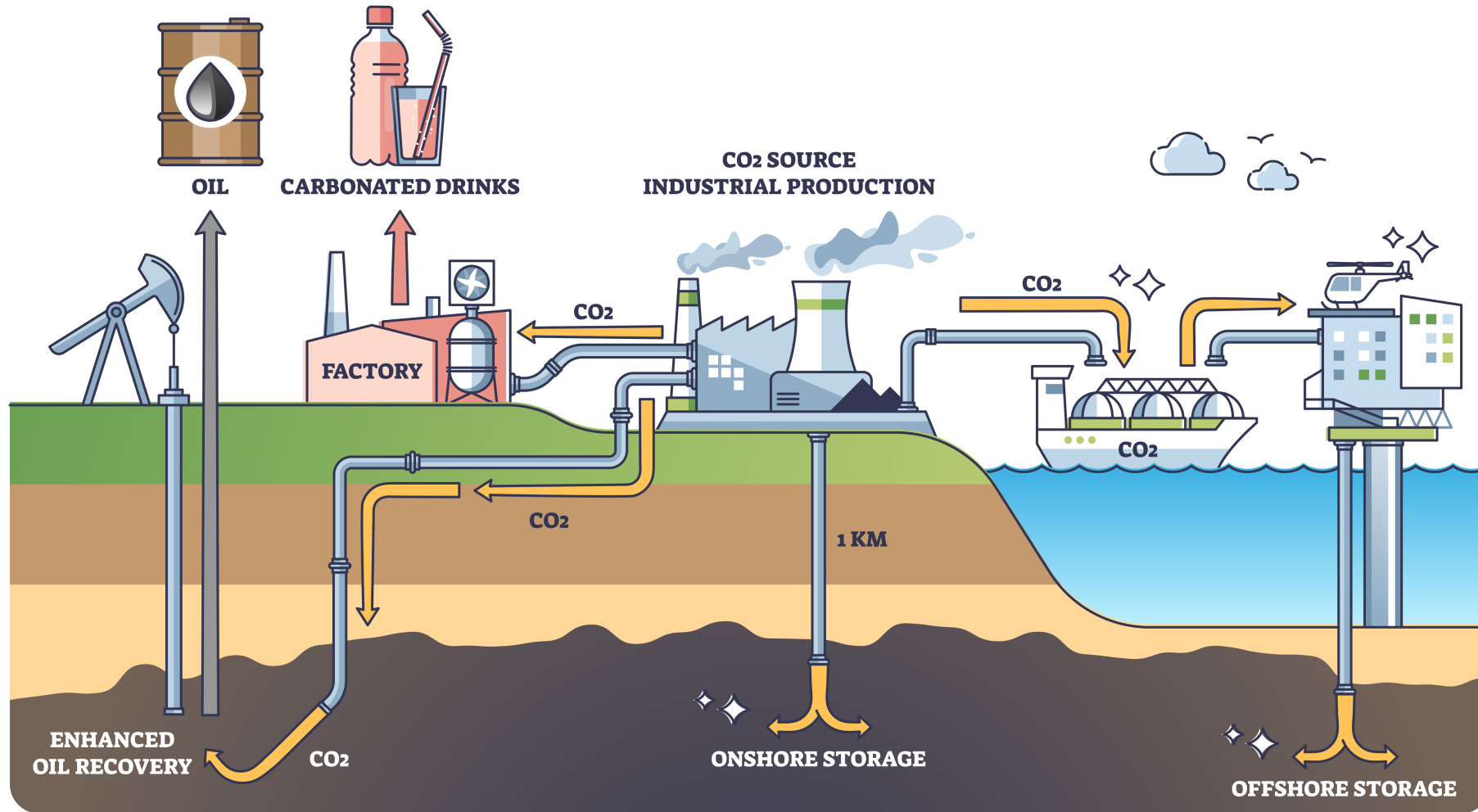
Prof. Jean-François
Molinari,
Computational Solid
Mechanics Laboratory,
EPFL



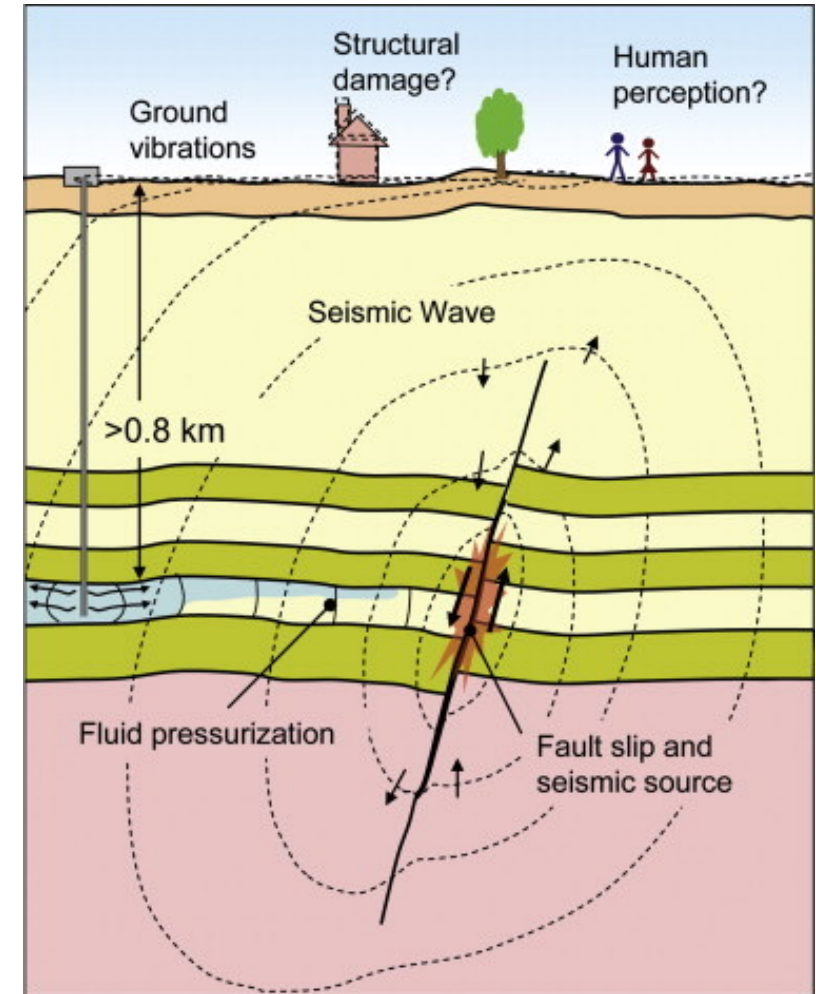
Dr. Nicolas Richart
HPC Application
Expert / Scientist,
Computational Solid
Mechanics Laboratory,
EPFL



Dr. Guillaume Anciaux
Research Associate,
Computational Solid
Mechanics Laboratory,
EPFL



Environmental risks: Surface Uplift / Subsidence & Induced Seismicity



From [Rutqvist et al, 2014]

Project goals

- Geomechanical evaluation of a potential CO2 storage sites
- Risks of fault activation and hydraulic fracturing
- Uplift and subsidence

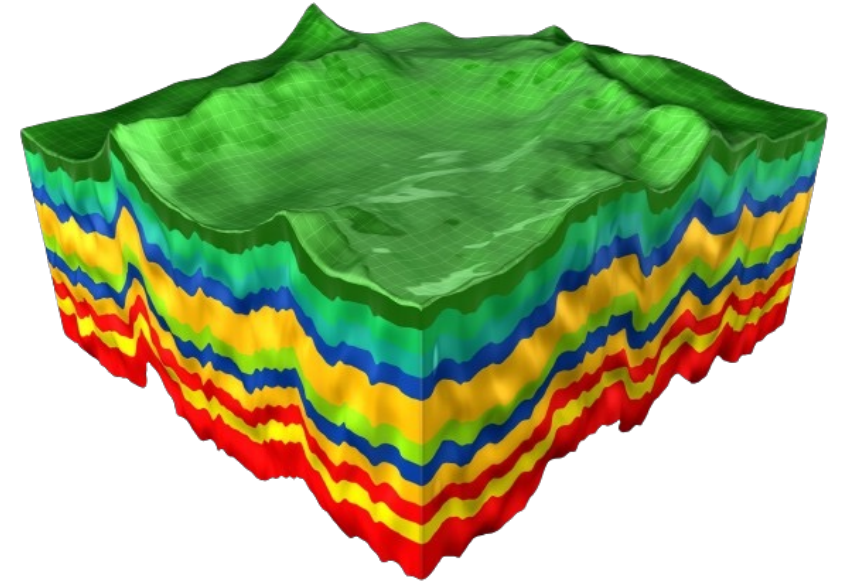
Methodology

- 3D Geomechanical simulator
- Fluid flow in the rock and along faults
- Deformations of the rock
- Opening and shearing of cracks and faults

Parallel open-source FE library Akantu www.akantu.ch, gitlab.com/akantu

Current assumptions:

- Single phase fluid flow
- Constant bulk and fault permeabilities
- Constant friction coefficient along faults



Governing equations for the rock (3D)

- Balance of momentum $\nabla \cdot \boldsymbol{\sigma}(u, p) + \mathbf{f} = 0$
- Fluid mass conservation $\frac{\partial \zeta(u, p)}{\partial t} + \nabla \cdot \mathbf{q}(u, p) = \gamma$

- Constitutive equations (w.r.t. initial state)

- Stress state

$$\boldsymbol{\sigma} = \mathbb{C}\boldsymbol{\varepsilon}(u) + \boldsymbol{\alpha}p$$

- Variation in fluid content

$$\zeta = \boldsymbol{\alpha} : \boldsymbol{\varepsilon}(u) + \frac{1}{M}p$$

- Darcy flow

$$\mathbf{q} = -\boldsymbol{\kappa}(u, p)\nabla p$$

- System to solve after implicit time integration

$$\begin{bmatrix} \mathbb{K} & \mathbb{A}_{p \rightarrow u} \\ \mathbb{A}_{u \rightarrow p}/\Delta t & \mathbb{S}/\Delta t + \mathbb{C} \end{bmatrix} \begin{bmatrix} \partial u \\ \partial p \end{bmatrix} = \begin{bmatrix} f_{n+1} - \mathbb{K}u_n - \mathbb{A}_{p \rightarrow u}p_n \\ \gamma_{n+1} - \mathbb{C}p_n \end{bmatrix}$$

Governing equations for faults and cracks (2D)

▪ Continuity of tractions $\boldsymbol{\sigma}'(u, p)\mathbf{n} = -\mathbf{t}$

▪ Lubrication flow $\frac{\partial w}{\partial t} + wS_f \frac{\partial p_f}{\partial t} + \nabla_{\parallel} \cdot (w\mathbf{q}_{\parallel}) + q_{-}^{\perp} + q_{+}^{\perp} = \gamma_f$

▪ Constitutive equations

• Traction
$$\mathbf{t} = \begin{cases} 0 & \text{if } \delta_n > 0 \\ \mathcal{N}(\boldsymbol{\delta}) & \text{if } \delta_n \leq 0 \end{cases}$$

• Coulomb friction
$$\|\boldsymbol{\tau}\| \leq f\boldsymbol{\sigma}'_n$$

• Darcy flow
$$\mathbf{q}_{\parallel} = -\frac{k_f}{\mu} \nabla_{\parallel} p_f$$

- 1st order FEs for flow and deformations
- Cohesive elements for cracks & faults [Camacho & Ortiz, 1996]
- Flow in a crack is averaged along width
- 2-node interface flow formulation after [Segura & Carol, 2004]

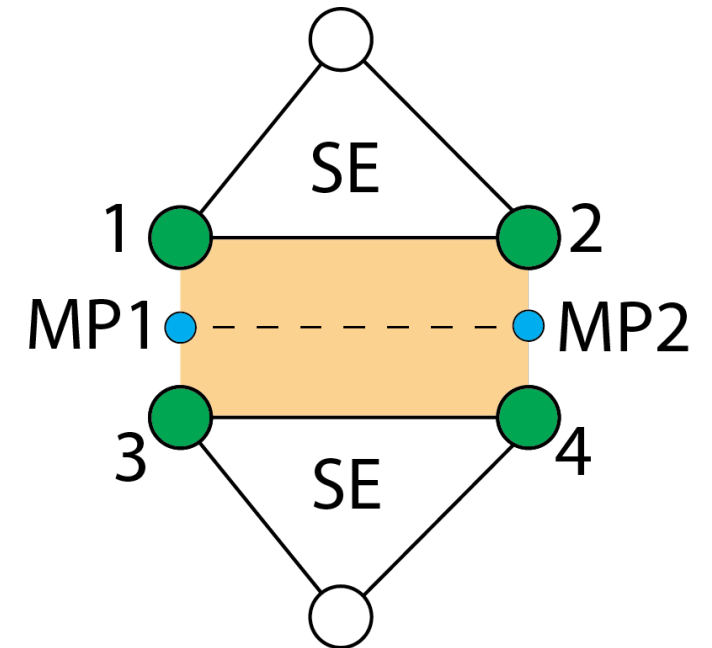
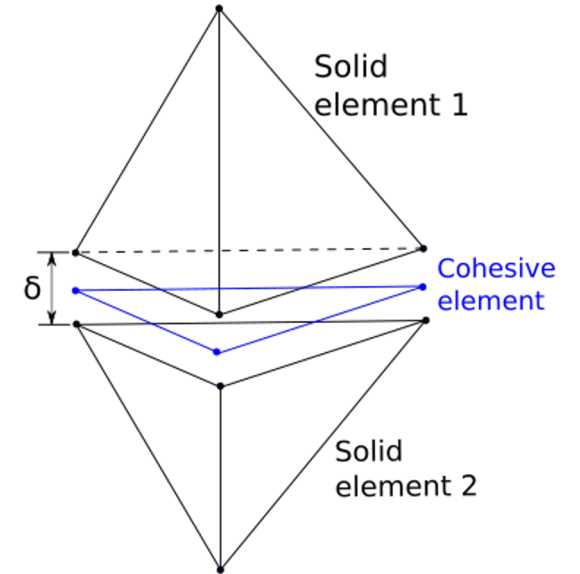
- Longitudinal flow

$$Q_{Lmp} = \frac{1}{2} \mathbf{K}_{Lmp} \cdot [\mathbb{I}; \mathbb{I}] \cdot \mathbf{p}$$

$$\mathbf{K}_{Lmp} = \iint_S \hat{k}_l \mathbf{B} \cdot \mathbf{B}^T dsdt$$
- Transversal flow

$$Q_{Tmp} = \mathbf{K}_{Tmp} \cdot [\mathbb{I}; -\mathbb{I}] \cdot \mathbf{p}$$

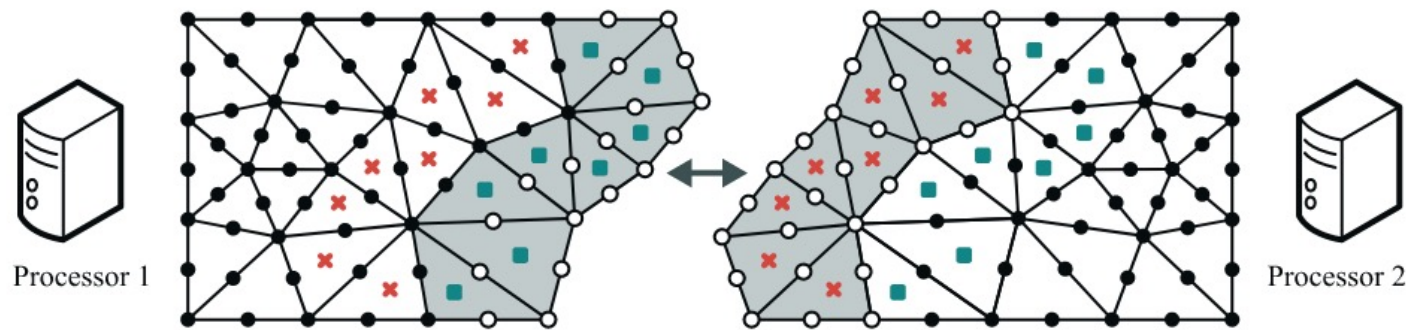
$$\mathbf{K}_{Tmp} = \iint_S k_t \mathbf{N} \cdot \mathbf{N}^T dsdt$$



Solution scheme and numerical details

$$\begin{bmatrix} \mathbb{K} & \mathbb{A}_{p \rightarrow u} \\ \mathbb{A}_{u \rightarrow p} / \Delta t & \mathbb{S} / \Delta t + \mathbb{C} \end{bmatrix} \begin{bmatrix} \partial u \\ \partial p \end{bmatrix} = \begin{bmatrix} \mathbf{f}_{n+1} - \mathbb{K} \mathbf{u}_n - \mathbb{A}_{p \rightarrow u} p_n \\ \gamma_{n+1} - \mathbb{C} p_n \end{bmatrix}$$

- Solution of nonlinear system by Newton Raphson
- Monolithic solve of Jacobian system by iterative partitioned conjugate gradient [[Prevost, 1997](#)]
- Parallel direct solver of linear subsystem (MUMPS)
- MPI parallelization & synchronization at the quadrature points

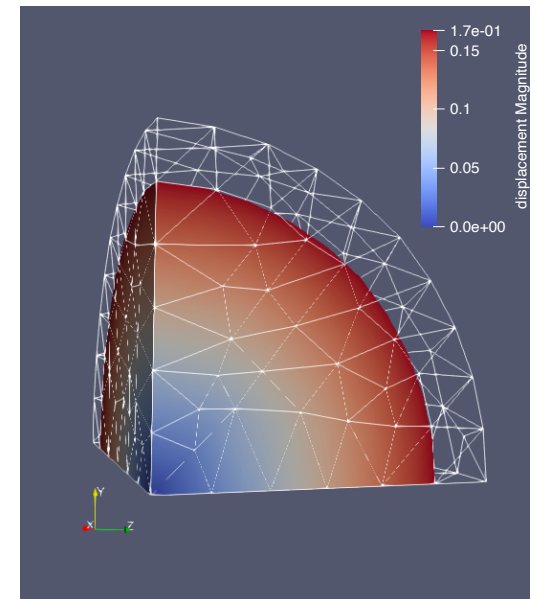
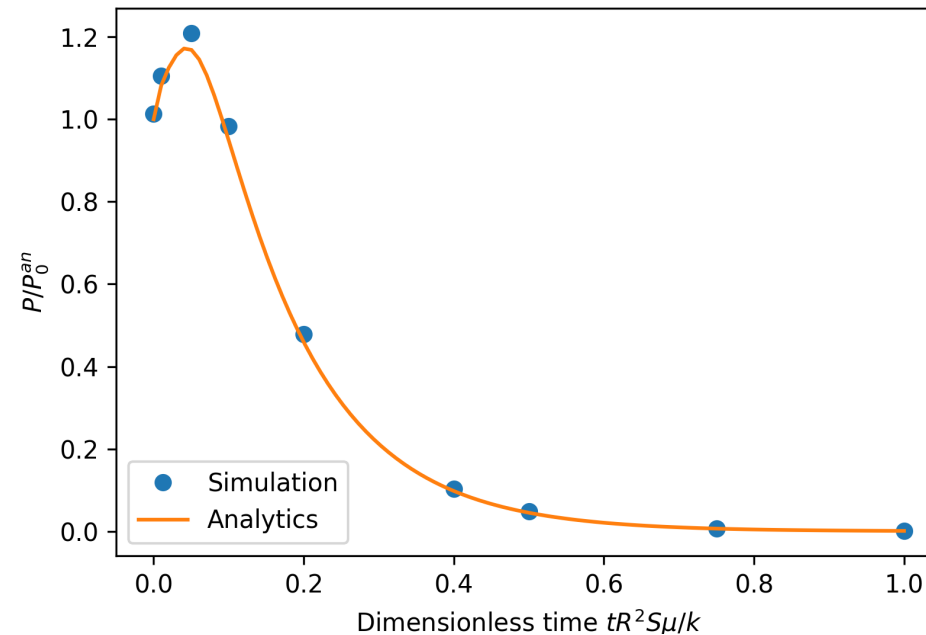
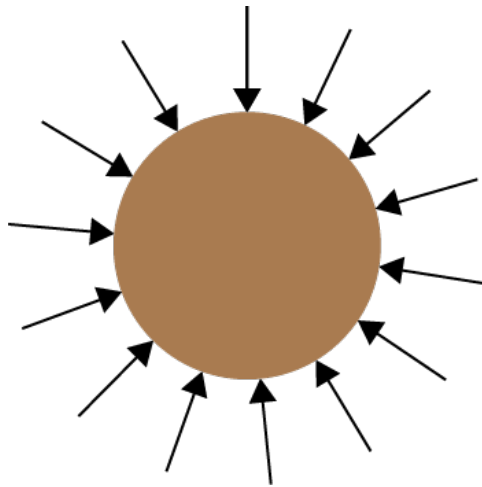


From [[Vocialta & Molinari, IJNME 2017](#)]

Benchmark

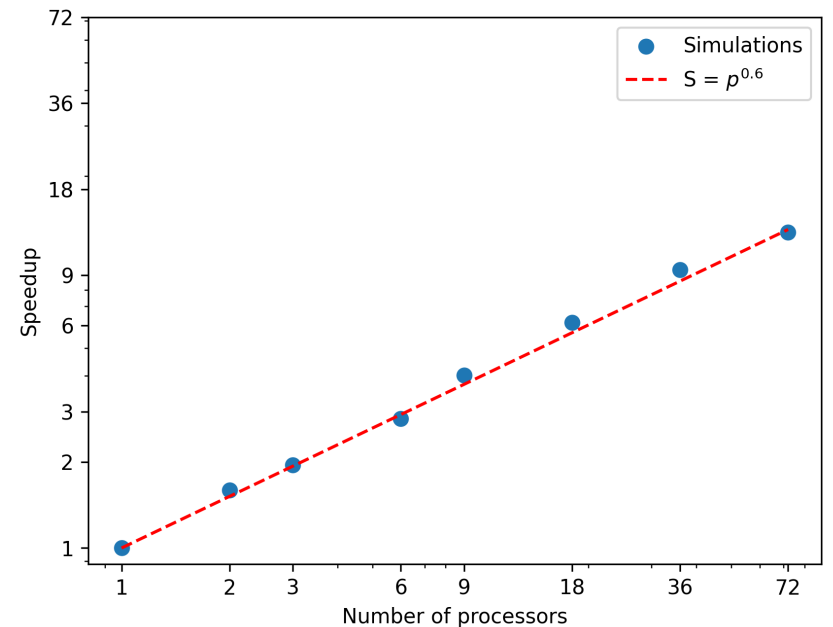
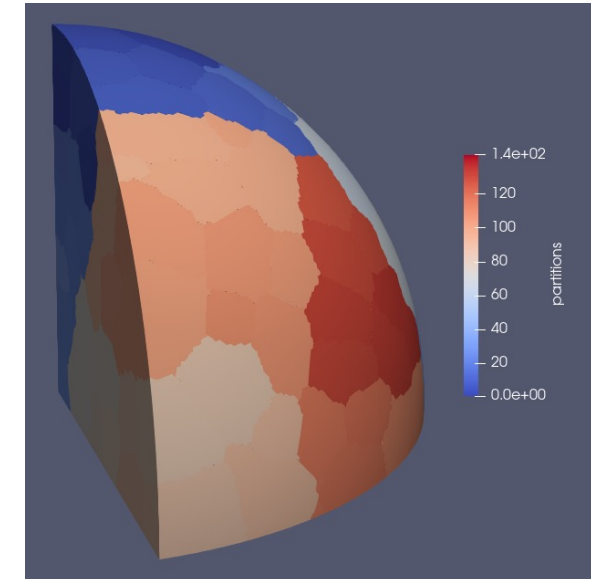
Poroelasticity

- Compression of saturated porous sphere [Cryer, 1963]
- Initial uniform pressure rise p^0
- Non-monotonic pressure diffusion – Mandel-Cryer effect
- Caused by stresses redistribution upon drainage

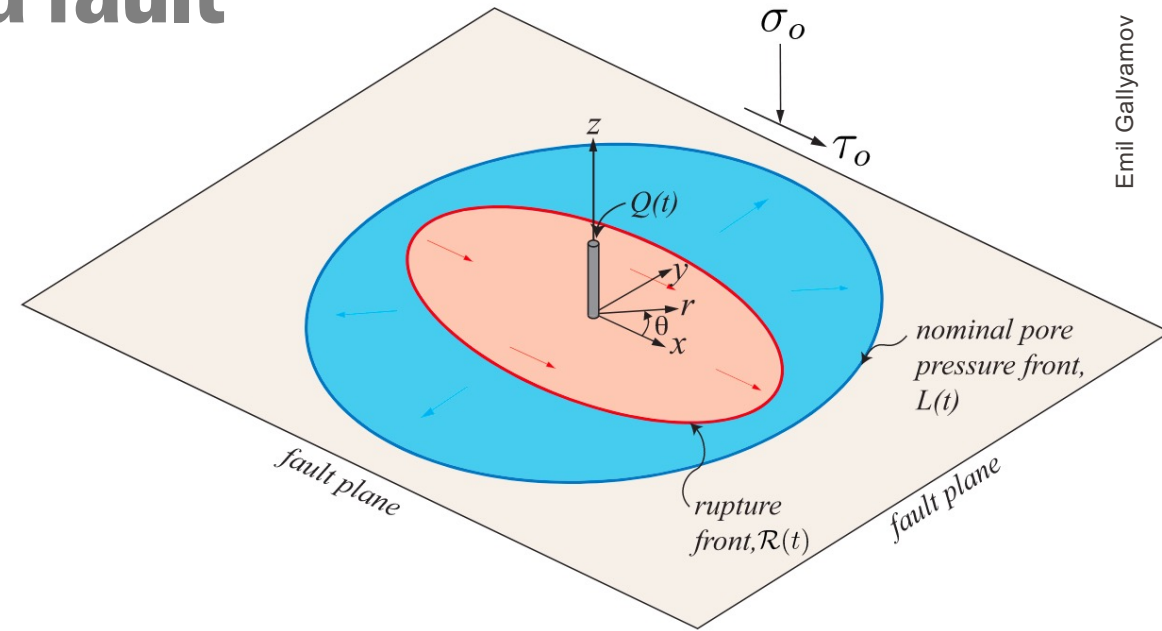


Strong scaling

- Scaling testing on a Cryer sphere with 1,200,000 DOFs
- From 1 up to 72 cores
- Intel Xeon nodes with 2 sockets of 36 cores, 512 Gb RAM and dual 25 Gb Ethernet links
- Speedup $S = T_1/T_p$
- Code scales with exponent of 0.6 (1 for perfect scaling)

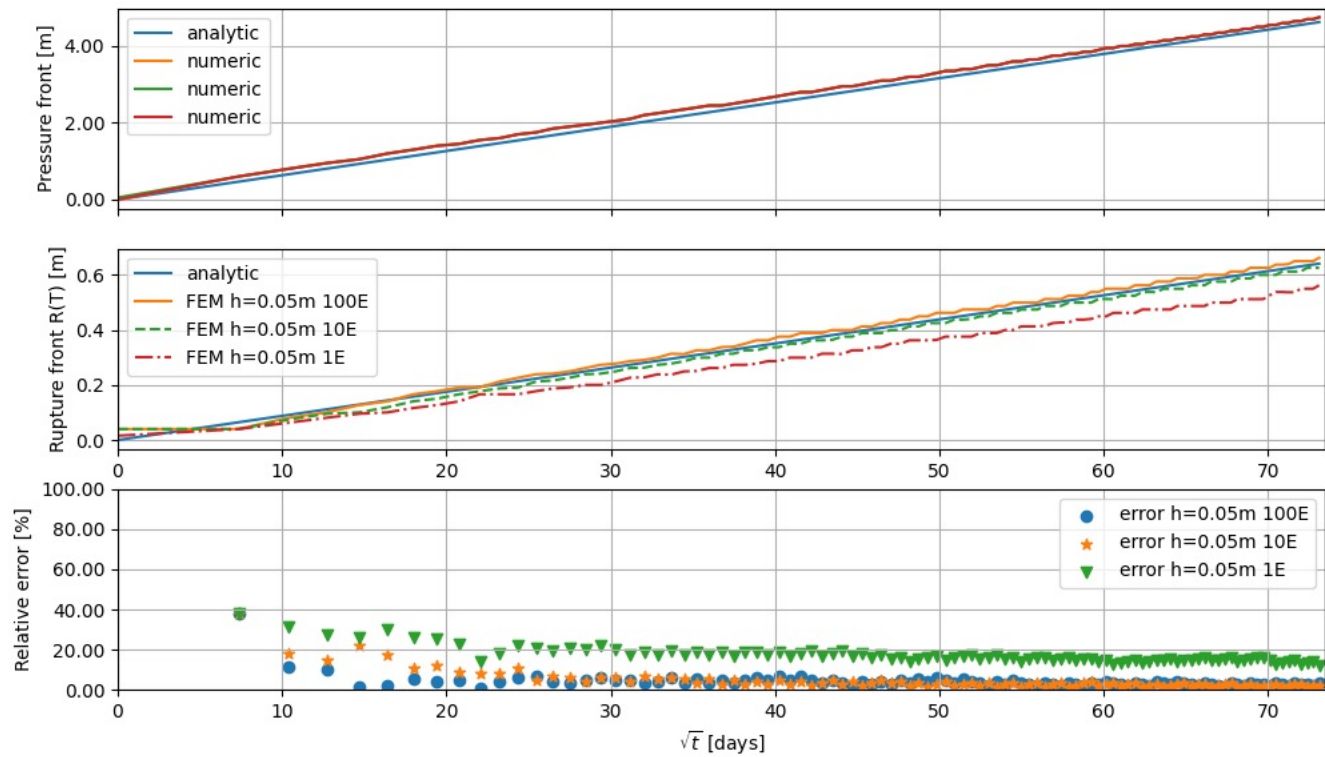
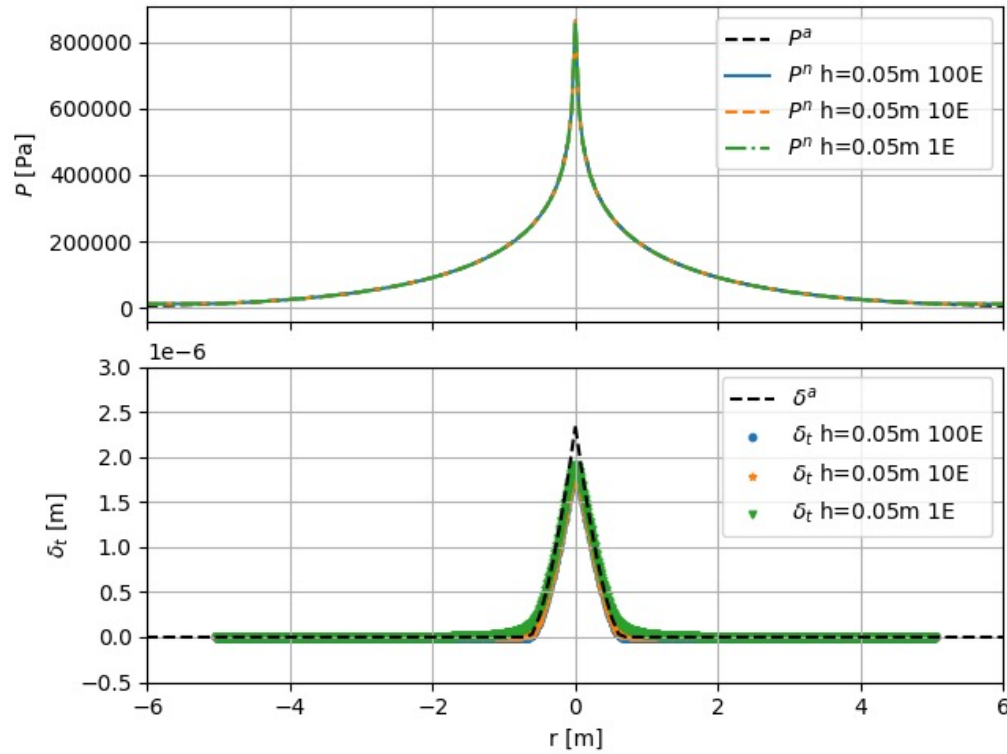
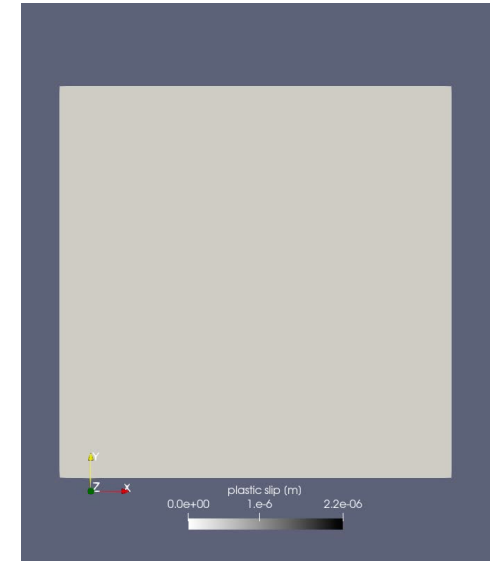
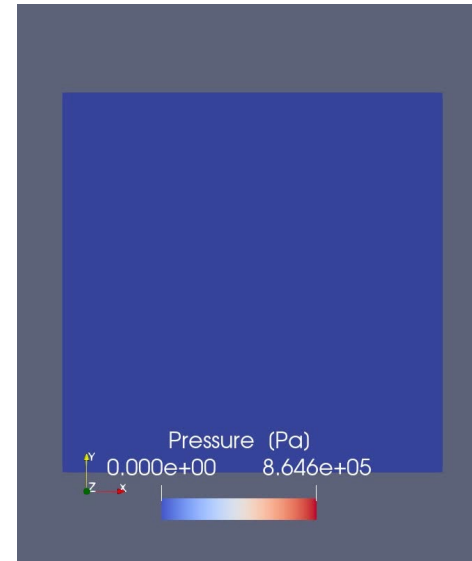


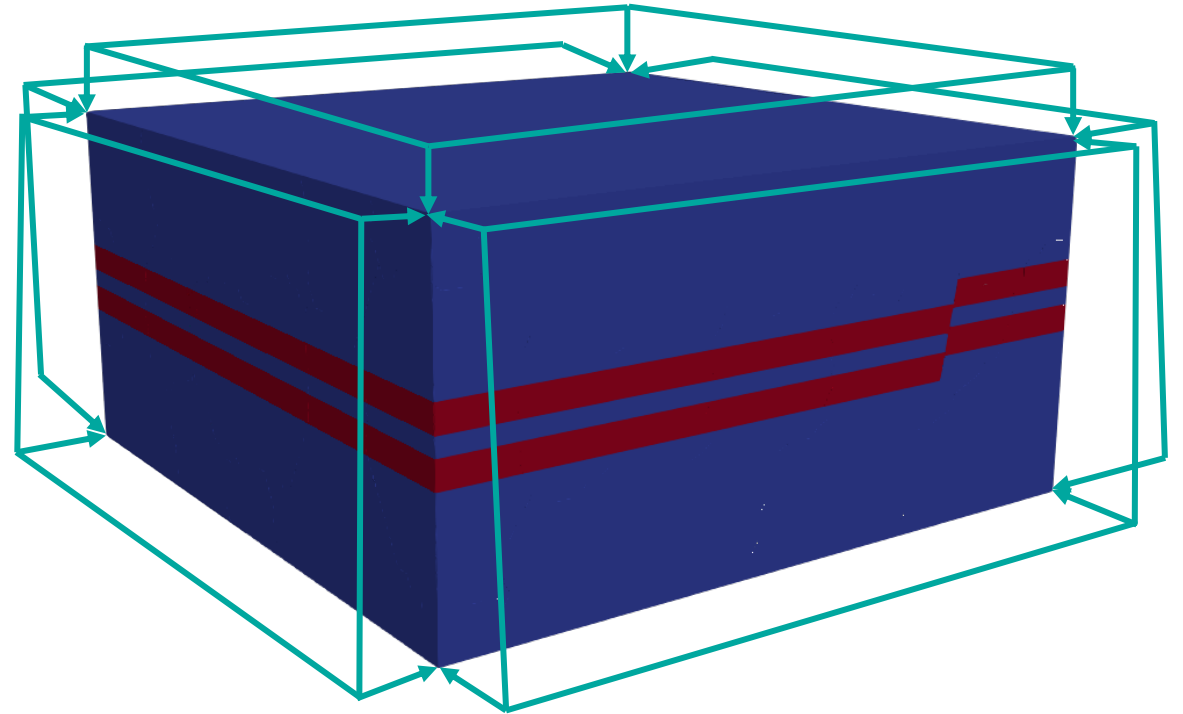
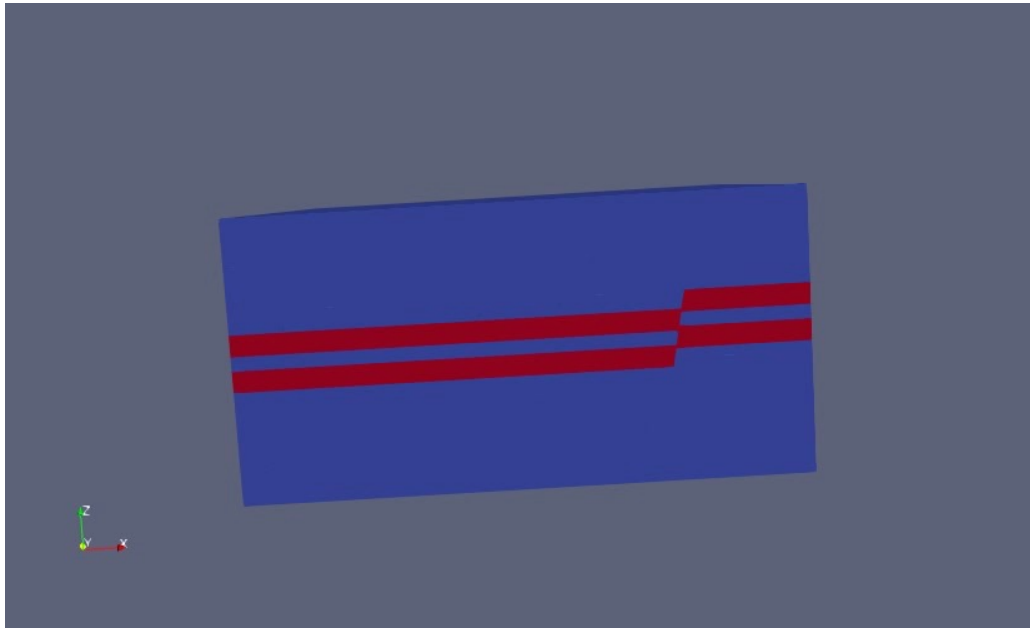
- Friction along a fault
- Point injection into a planar fault
- Fault is under normal and shear stress
- Coulomb friction along the fault
- Pressure diffusion causes evolution of the rupture front
- Stable (aseismic) rupture propagation
- Analytical solution in [\[Saez et al., JMPS 2022\]](#)



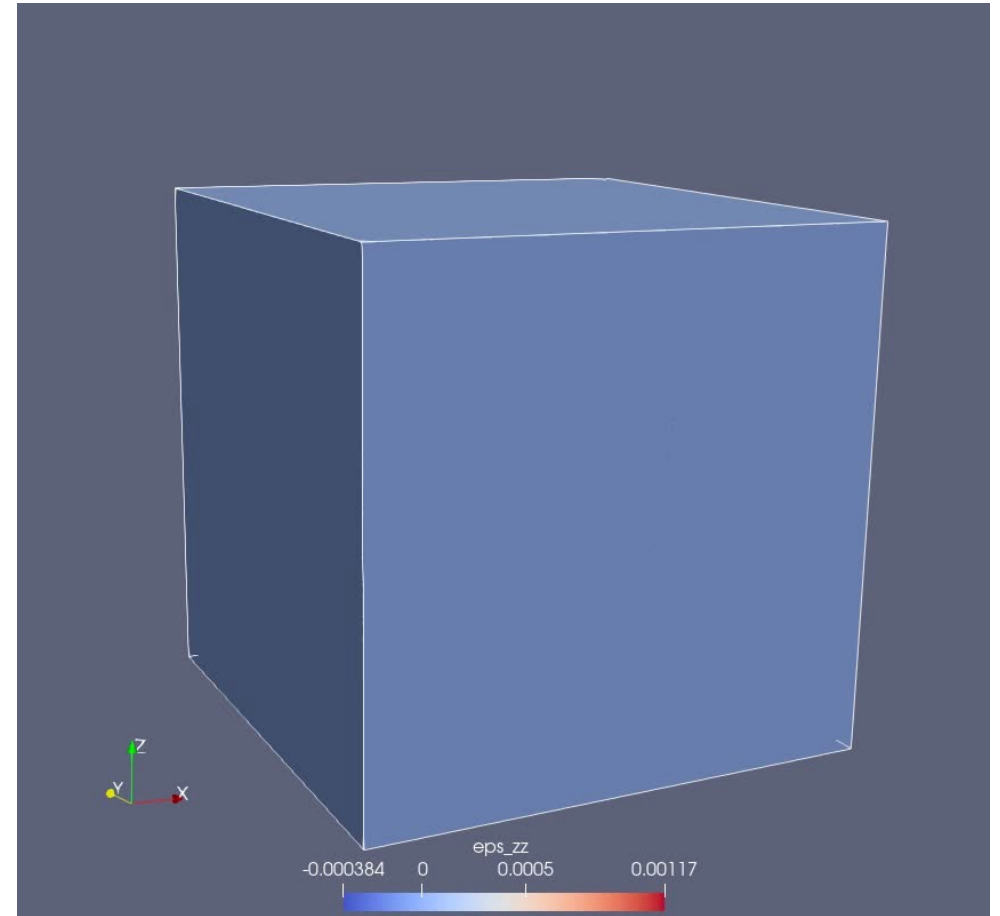
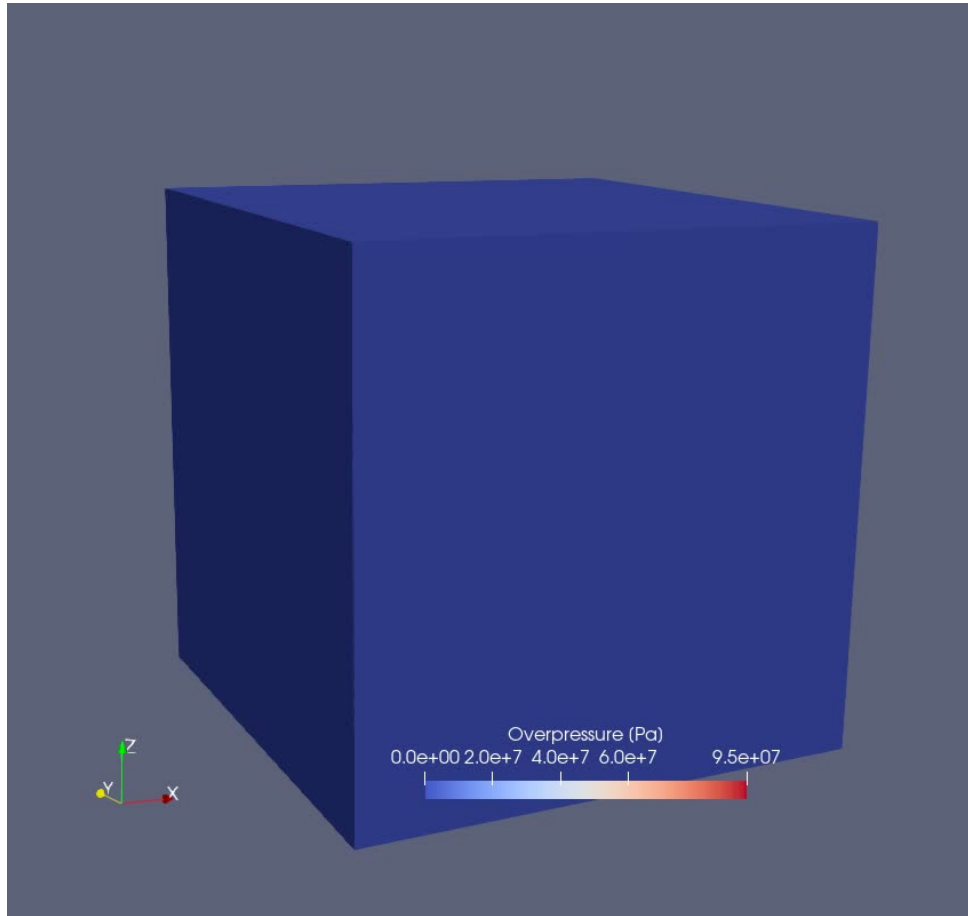
From [\[Saez et al., JMPS 2022\]](#)

Injection into a fault

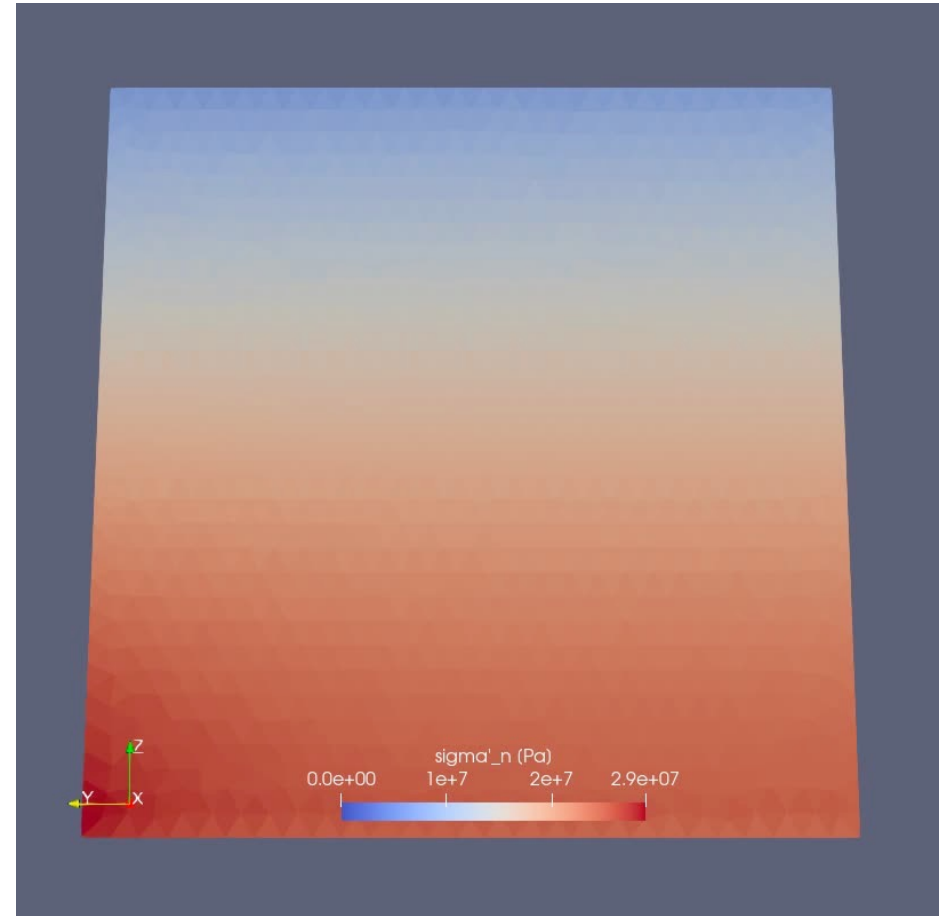
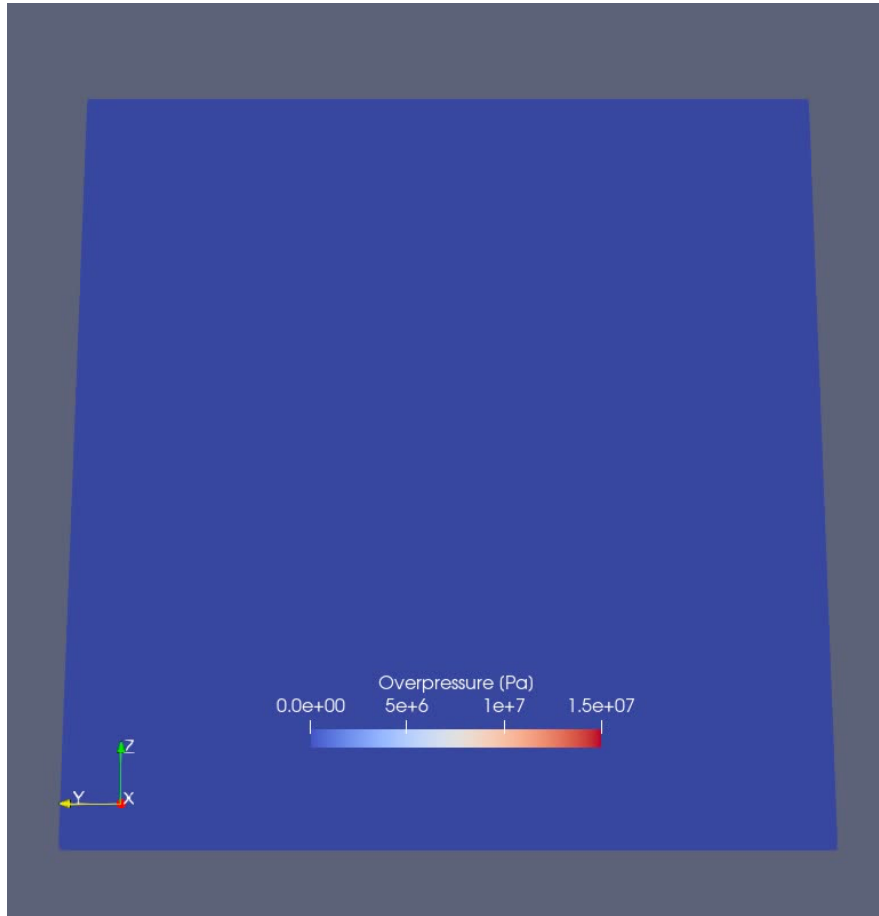
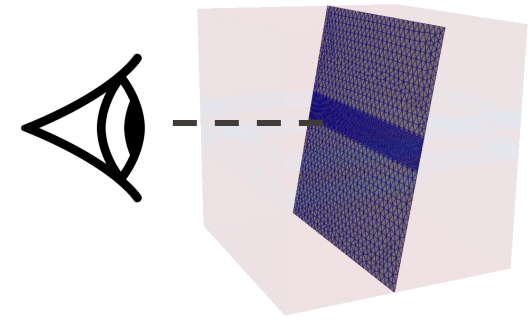




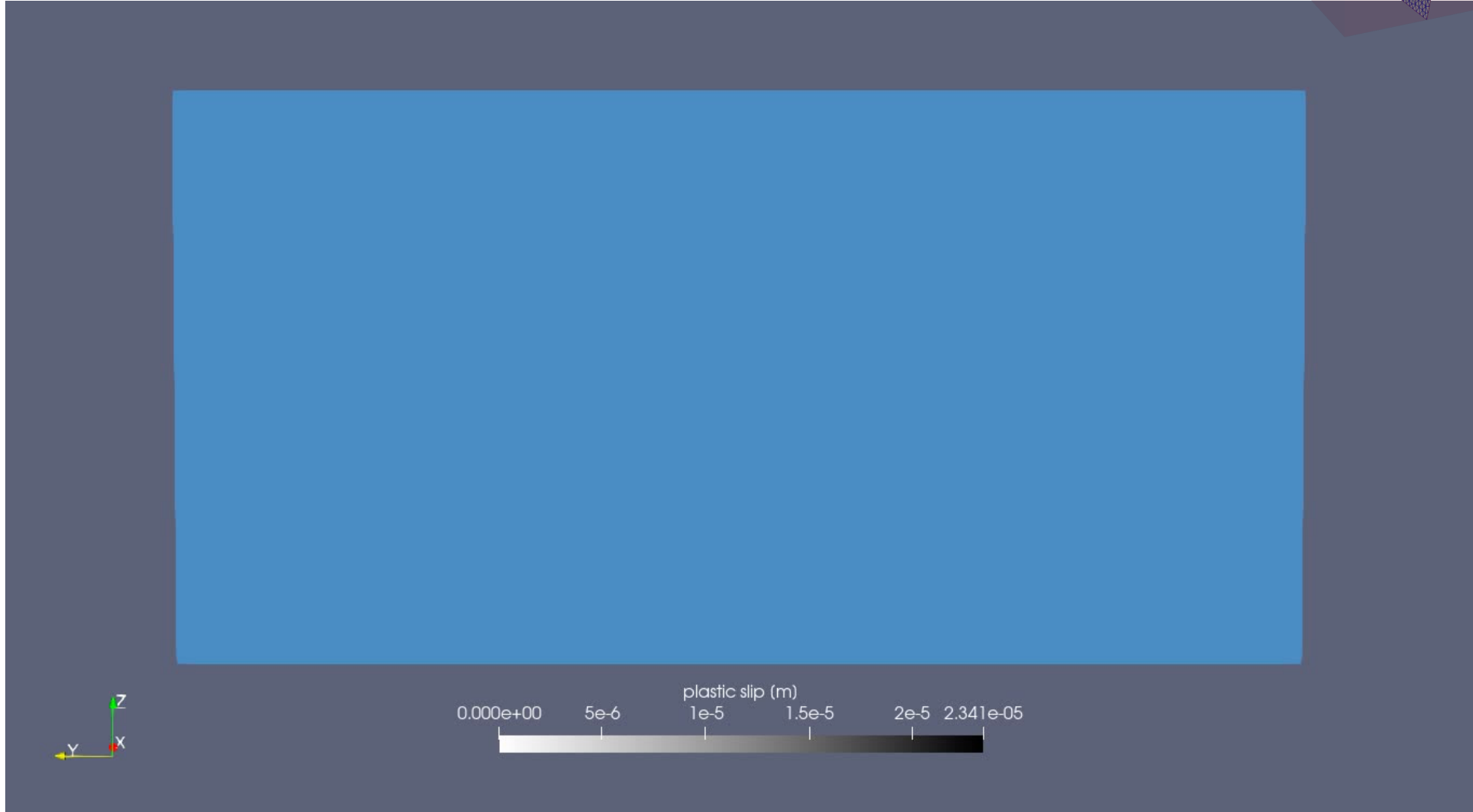
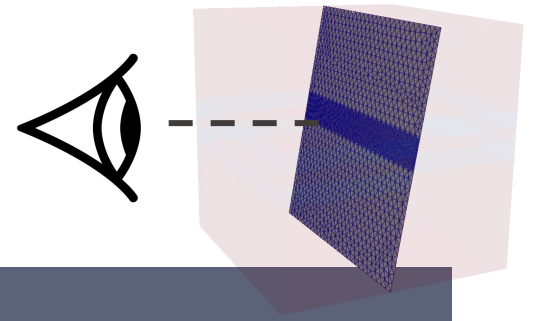
Overpressure and deformations



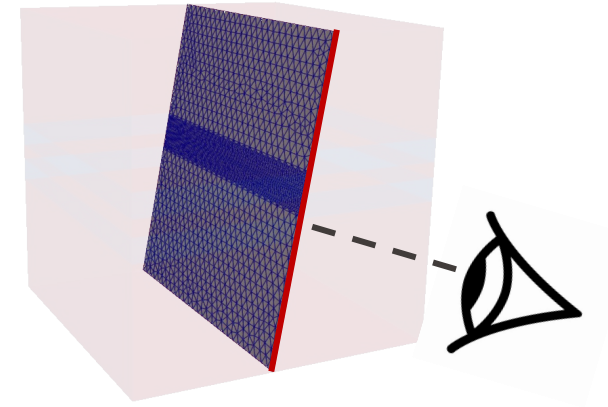
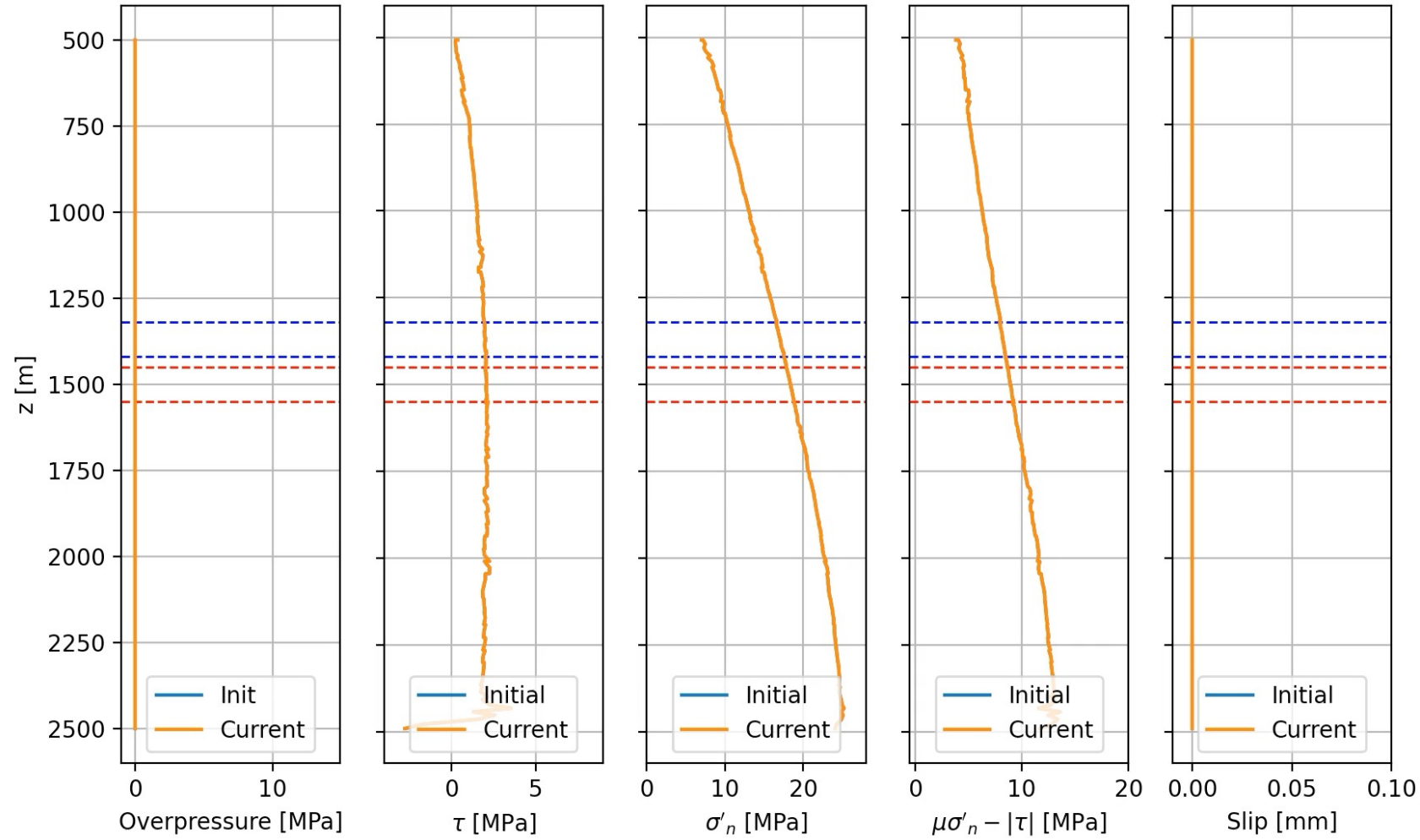
Fault overpressure and stresses



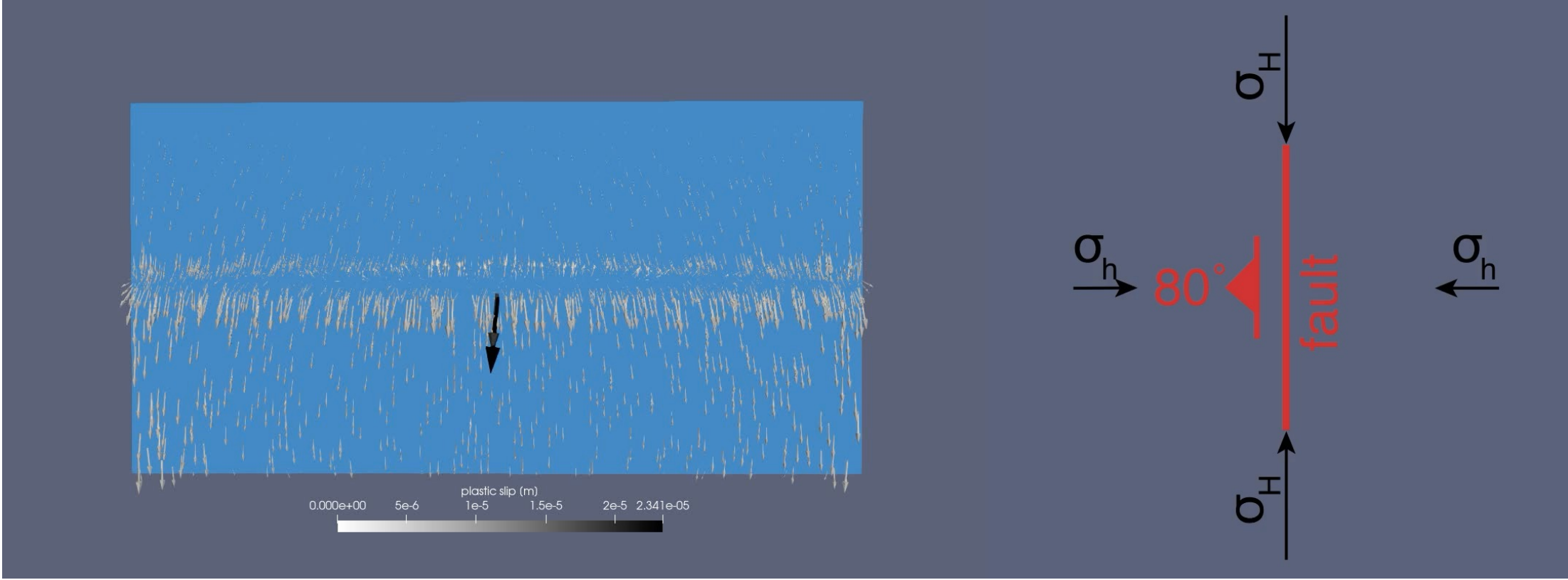
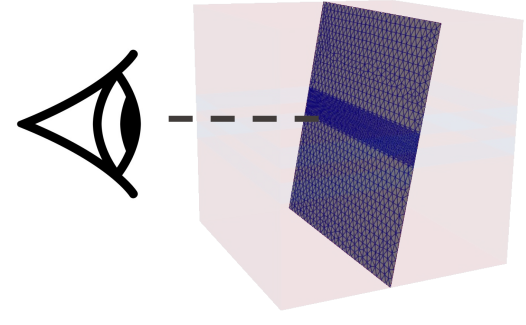
Slip



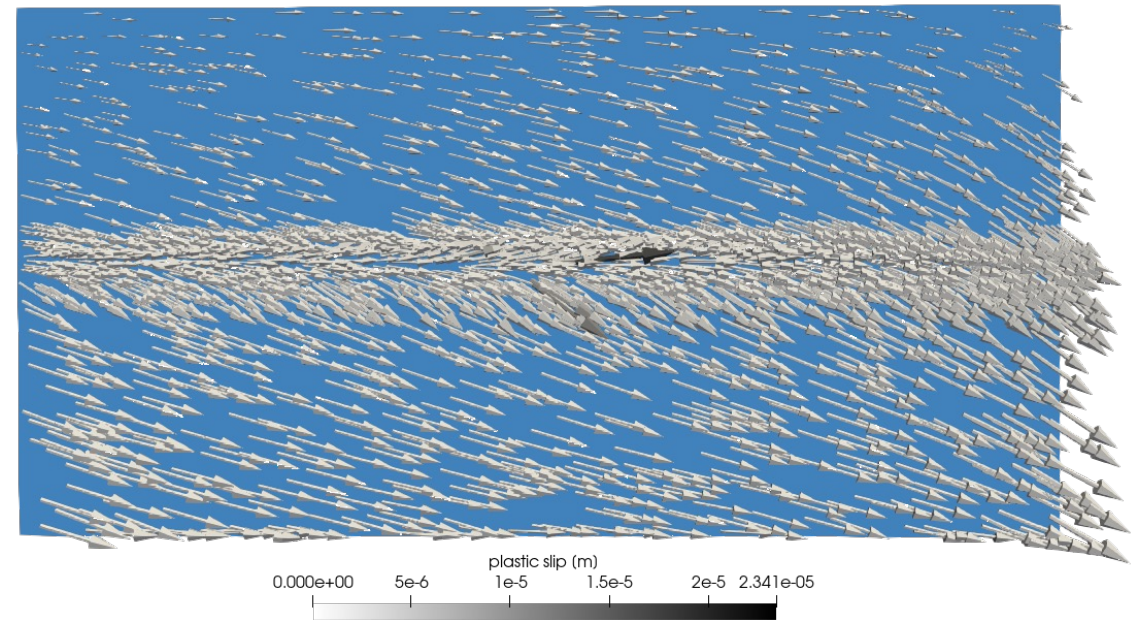
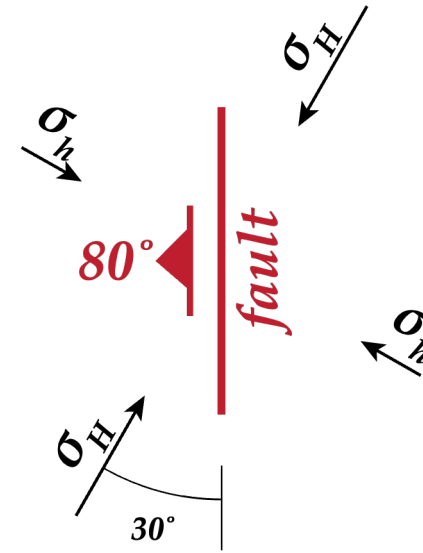
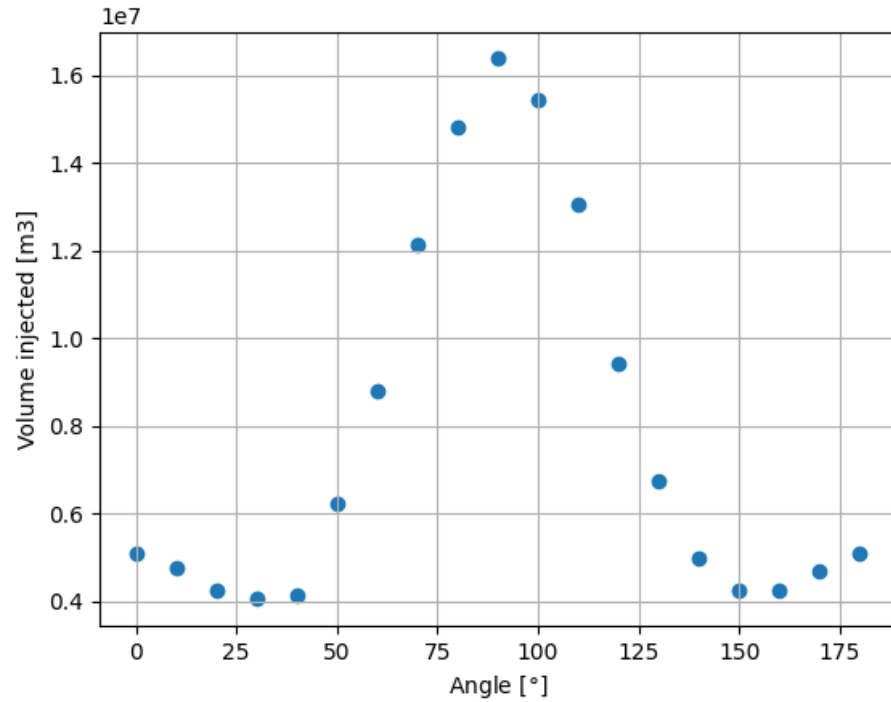
Quantitative evaluation



Slip vs stress orientation



Critical stress orientations



Summary

- Fully-coupled geomechanical simulator was developed
- MPI parallelization allows to solve large geological models
- Helps to evaluate fault slip initiation, aseismic slip, poroelastic effects
- Benchmarked against multiple analytical solutions for flow, solid mechanics, friction and hydro-shearing
- Capacities were demonstrated in the injection into a faulted aquifer scenario

Outlook:

- Investigating the effect of poroelasticity on aseismic slip
- Adding opening-dependent fault permeability
- Coupling with a multi-phase reservoir simulator
- Adding thermal effects into the model

- Richart, N., & Molinari, J. F. (2015). Implementation of a parallel finite-element library: Test case on a non-local continuum damage model. *Finite Elements in Analysis and Design*, 100, 41–46.
- Camacho, G. T., & Ortiz, M. (1996). Computational modelling of impact damage in brittle materials. *International Journal of Solids and Structures*, 33(20–22), 2899–2938.
- Segura, J. M., & Carol, I. (2004). On zero-thickness interface elements for diffusion problems. *International Journal for Numerical and Analytical Methods in Geomechanics*, 28(9), 947–962.
- Prevost, J. H. (1997). Partitioned solution procedure for simultaneous integration of coupled-field problems. *Communications in Numerical Methods in Engineering*, 13(4), 239–247.
- Vocialta, M., & Molinari, J.-F. (2015). Influence of internal impacts between fragments in dynamic brittle tensile fragmentation. *International Journal of Solids and Structures*, 58, 247–256.
- Sáez, A., Lecampion, B., Bhattacharya, P., & Viesca, R. C. (2022). Three-dimensional fluid-driven stable frictional ruptures. *Journal of the Mechanics and Physics of Solids*, 160, 104754.
- Jha, B., & Juanes, R. (2014). Coupled multiphase flow and poromechanics: A computational model of pore pressure effects on fault slip and earthquake triggering. *Water Resources Research*, 50(5), 3776–3808.
- Rutqvist, J., Cappa, F., Rinaldi, A., Godano, M. (2014). Modeling of induced seismicity and ground vibrations associated with geologic CO₂ storage, and assessing their effects on surface structures and human perception. *International Journal of Greenhouse Gas Control*, 24, 64-77.